Vehicle Performance

Pierre Duysinx Research Center in Sustainable Automotive Technologies of University of Liege Academic Year 2021-2022

Part 1: Tractive efforts and road loads

Outline

DESCRIPTION OF VEHICLE MOTION

- Longitudinal motion
- POWER AND TRACTIVE FORCE AT WHEELS
 - Transmission efficiency
 - Gear ratio
 - Expression of power and forces at wheels
 - Power and forces diagram
- VEHICLE RESISTANCE
 - Aerodynamic
 - Rolling resistance
 - Grading resistance
 - General expression of vehicle resistance forces

Outline

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 - Maximum speed
 - Gradeability and maximum slope
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 - Acceleration time and distance

Outline

- FUEL CONSUMPTION AND EMISSIONS
 - Specific consumption of power plant
 - Vehicle fuel consumption measures
 - Constant speed consumption
 - Variable speed consumption and driving cycles
 - Chassis dynamometer

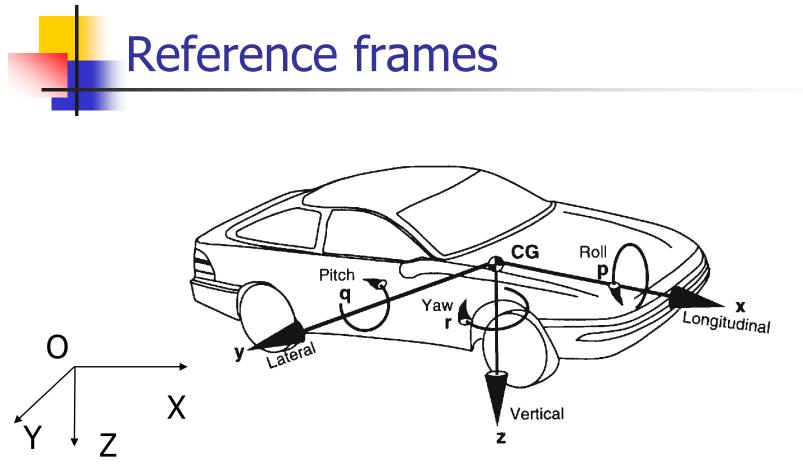
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Assumptions and definitions

Assumptions

- The vehicle is made of several components or subsystems
- We consider the motion of the system as a whole
- During acceleration, braking, turn, the vehicle is considered as a rigid body motion and is characterized by its geometry, its mass and inertia properties

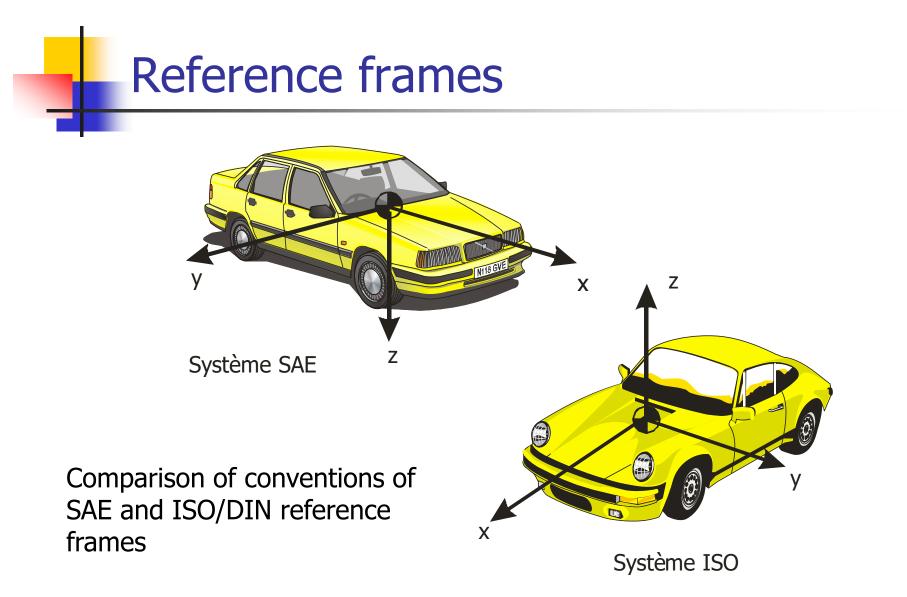


Inertial coordinate system OXYZ

Local reference frame oxyz attached to the vehicle body -SAE (Gillespie, fig. 1.4)

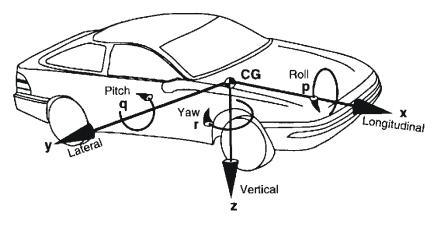
Reference frames

- Inertial reference frame
 - X direction of initial displacement or reference direction
 - Y right side travel
 - Z towards downward vertical direction
- Vehicle reference frame (SAE):
 - x along motion direction and vehicle symmetry plane
 - z along vertical direction pointing to the center of the earth
 - y in the lateral direction on the right-hand side of the driver towards the downward vertical direction
 - o, origin at the center of mass



Local velocity vectors

- Vehicle motion is often studied in car-body local systems
 - u forward speed (+ if in front)
 - v side speed (+ to the right)
 - w vertical speed (+ downward)
 - p rotation speed about x axis (roll speed)
 - q rotation speed about y (pitch)
 - r rotation speed about z (yaw)

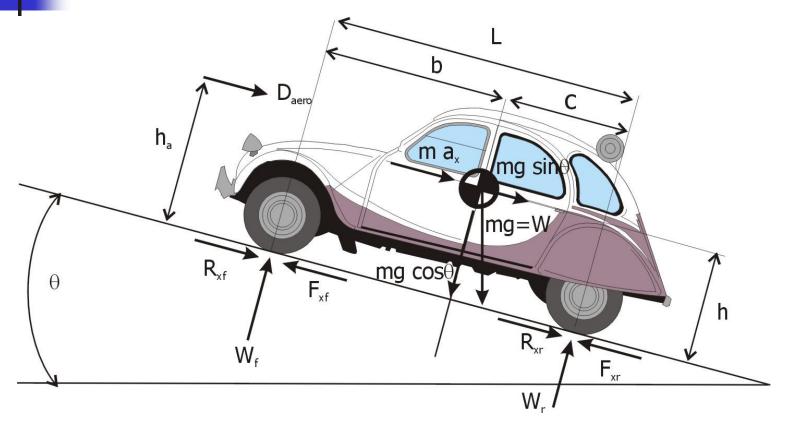


Forces

- Forces and moments are accounted positively when acting onto the vehicle and the positive direction with respect to the considered frame
- Corollary
 - A positive F_x force is propelling the vehicle forward
 - The reaction force of the ground onto the wheels is accounted negatively.
- Because of the inconveniency of this definition, the SAEJ670e « Vehicle Dynamics Terminology » is naming as normal force a force acting downward while vertical forces are referring to upward forces

Equilibrium of longitudinal motion

Longitudinal motion



 $ma_x = (F_{xf} + F_{xr}) - (R_{xf} + R_{xr}) - mg\sin\theta - F_{AERO}$

Longitudinal equilibrium

Equilibrium along forward x direction

 $ma_x = (F_{xf} + F_{xr}) - (R_{xf} + R_{xr}) - mg\sin\theta - F_{AERO}$

Equation of vehicle longitudinal motion

$$ma_x = F_t - F_{RR} - mg\sin\theta - F_{AERO}$$

Or
$$\boxed{ma_x = F_t - F_{RES}}$$

- Total tractive force $F_t = F_{xf} + F_{xr}$
- Total road resistance force $F_{RES} = F_{RR} + mg\sin\theta + F_{AERO}$

Newton's law of motion

Newton's law for longitudinal motion:

$$F_t = F_{AERO} + F_{RR} + mg\sin\theta + m_e\frac{dV}{dt}$$

- The traction force $F_{\rm T}$ is used to face the resistance forces and to accelerate the vehicle
- Driving resistance forces:
 - Aerodynamics forces
 - Rolling resistance forces
 - Slope forces

Driving resistance forces

Aerodynamic drag

$$F_{AERO} = \frac{1}{2}\rho SC_x V^2$$

Rolling resistance forces

 $F_{RR} = mg\cos\theta f_{RR}$

Slope resistance

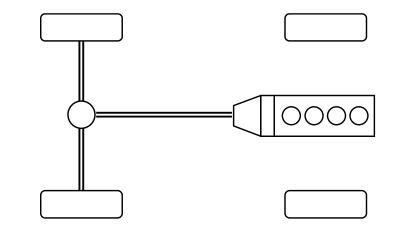
 $F_{SLOPE} = mg\sin\theta$

POWER AT WHEELS

The power that comes to the wheels is the engine power multiplied by the efficiency of the transmission efficiency η_t

$$\mathcal{P}_w = \eta_t \mathcal{P}_p$$

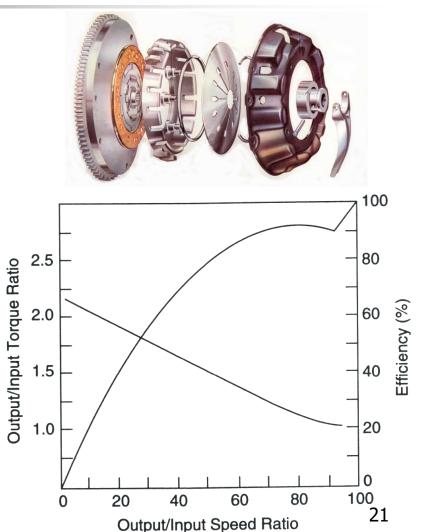
- The driveline efficiency η :
 - Clutch
 - Gear box
 - Differential and transfer box
 - Kinematic joints

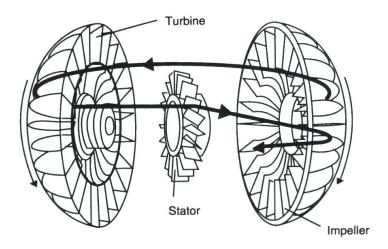


$$\eta_t = \eta_{clutch} \eta_{box} \eta_{dif} \eta_{joints}$$

Friction and hydraulic clutches

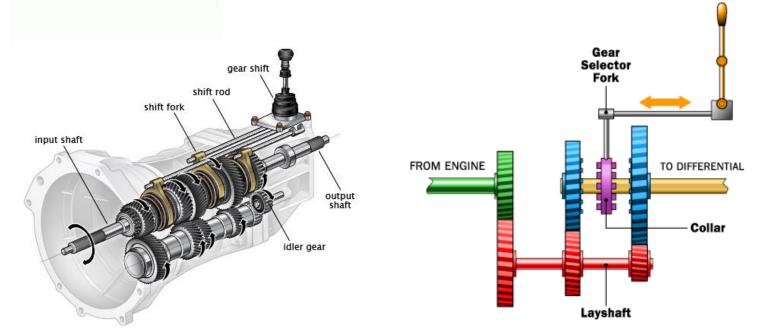
- Clutch efficiency
 - Friction clutch $\eta = 100\%$
 - Hydraulic coupler: η~90%





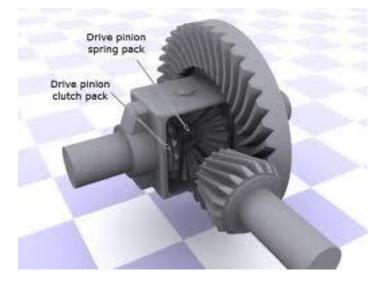
Power and tractive efforts at wheels

- Manual gearbox efficiency:
 - Efficiency of a pair of gear (good quality) η= 99% to 98.5 %
 - Gear box: double gear pairs: $\eta = 97.5\%$
 - Gear box: direct drive: $\eta = 100\%$



Differential system

- Efficiency of differential
 - Longitudinal layout: 90° change of direction (bevel pair) + offset of the shaft (hypoid gear): η = 97,5 %
 - Transversal layout: no bevel \rightarrow good quality gear pair: $\eta = 98,75\%$





Driveshafts

- Propeller shaft efficiency
 - The propeller shaft transmitting torque from the gearbox to the rear axle: 98%

$$\eta_{tm} = \eta_U^2 = 0.99^2 = 0.98$$



- Driveshaft efficiency: 98%
 - Constant velocity joints
 - Rzeppa
 - Tripod

 $\eta_{DS} = \eta_{RZP} \ \eta_{TRP} = 0.99^2 = 0.98$



Global efficiency in various situations

	Gear ratio	Longitudinal layout	Transversal layout
Friction clutch	Normal	1. 0,975. 0,975 = 0,95	1. 0,975 0,985 = 0,96
	Direct	1. 1. 0,975 = 0,975	Х
Hydraulic coupling	Normal	0,88 0,975 0,975 = 0,86	0,88 0,975 0,985 = 0,865
	Direct	0,88 1. 0,975 = 0,88	Х

WHEEL TRACTIVE EFFORT

Power at wheels and power at the plant

$$\mathcal{P}_t = F_t v \qquad \qquad \mathcal{P}_p = C_p \,\omega_p$$

Gear ratio i>1

$$\omega_p = i \,\omega_w \qquad \qquad i = i_{box} \,i_{dif} \qquad \qquad i = \frac{\omega_{in}}{\omega_{out}} > 1$$

Displacement speed and rotation speed of the wheels

$$v = \omega_w R_e$$

Re: effective rolling radius of the tire

(.1.

SPEED – ENGINE ROTATION SPEED RELATION

Relation between plant rotation speed and traveling speed

$$v = \frac{R_e}{i} \, \omega_p$$

- Transmission length R/i
 - Indicates the travelling speed for a given plant rotation speed.
 - Generally given in km/h per rpm of the plant
 - Example 30 km/h per 1000 tr/min

$$\frac{R_e}{i} = \frac{30/3, 6}{1000\ 2\ \pi/60} = 0,07958\ m$$

TRACTIVE FORCES

It follows

$$F_t v = \eta_t \ C_p \, \omega_p$$

$$F_t = \eta_t \ C_p \ \frac{\omega_p}{v}$$

Then the tractive force writes

$$F_t = \eta_t \ C_p \ \frac{\omega_p}{\omega_w R_e} = \eta_t \ C_p \ \frac{i}{R_e}$$

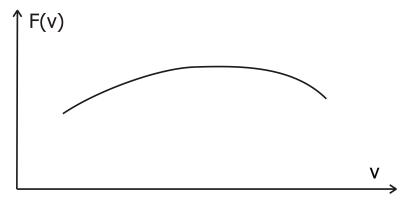
For a given speed v and a transmission ratio, one has the engine rotation speed:

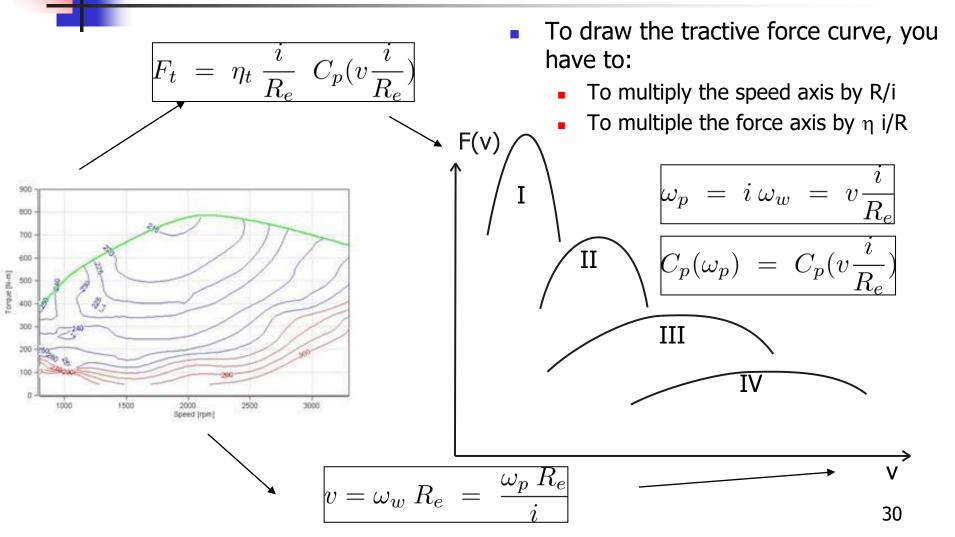
$$\omega_p = i \,\omega_w = v \frac{i}{R_e} \qquad \qquad C_p(\omega_p) = C_p(v \frac{i}{R_e})$$

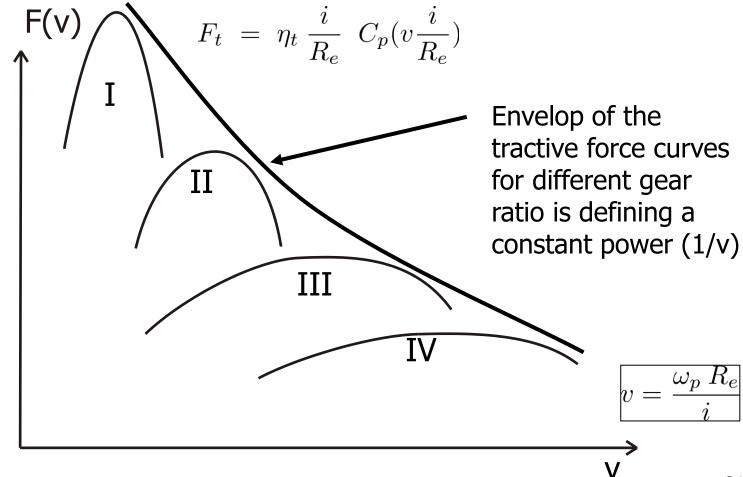
 So, for a given transmission ratio, one gets the tractive force in terms of the vehicle speed

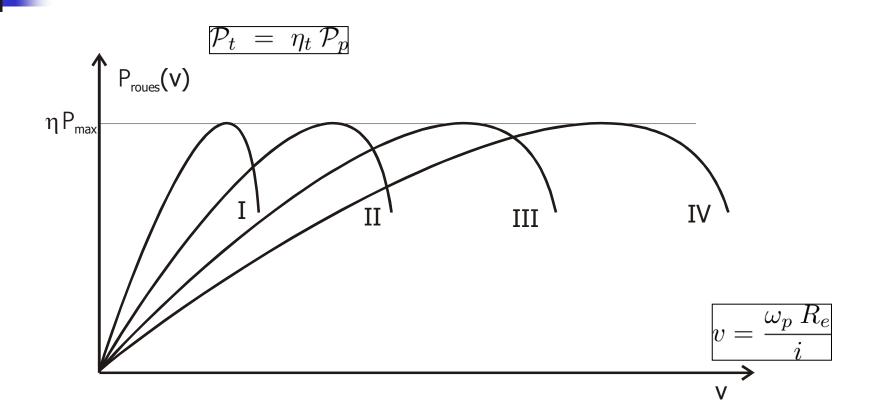
$$F_t = \eta_t \frac{i}{R_e} C_p(v \frac{i}{R_e})$$

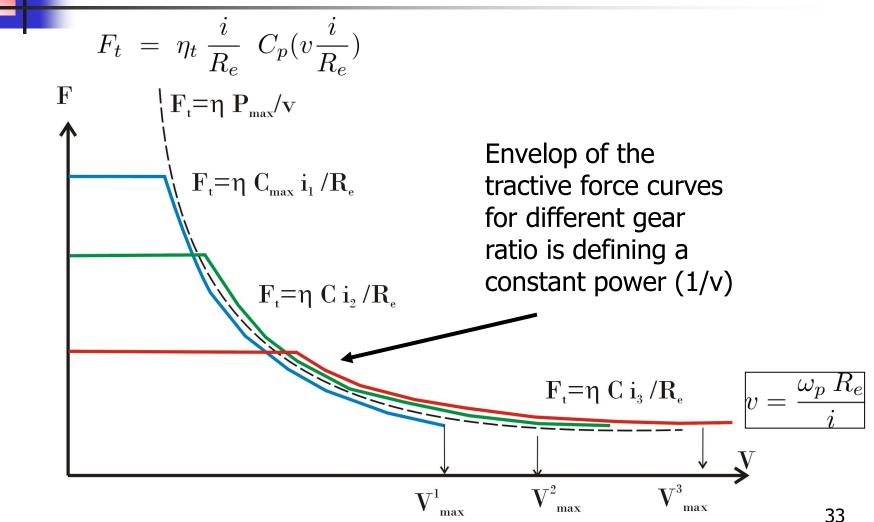
- Plotting the curves requires
 - Multiplying the speed curve by R/i
 - Multiplying the tractive force by η i/R

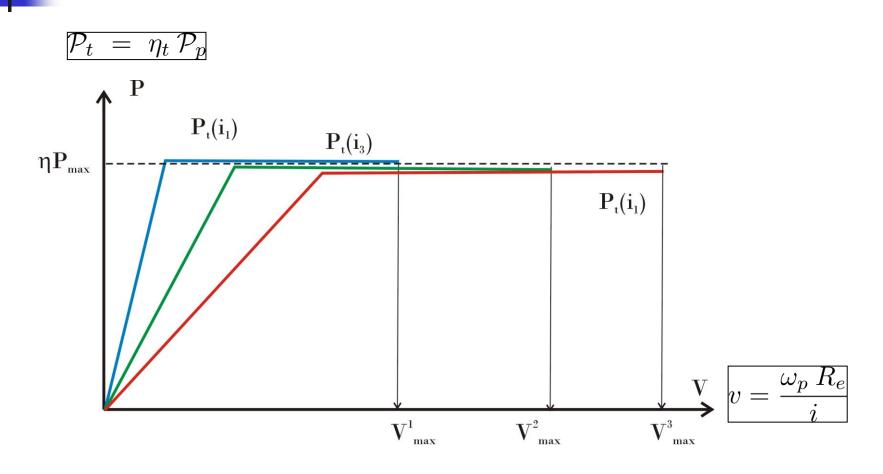












Vehicle resistance

Vehicle resistance

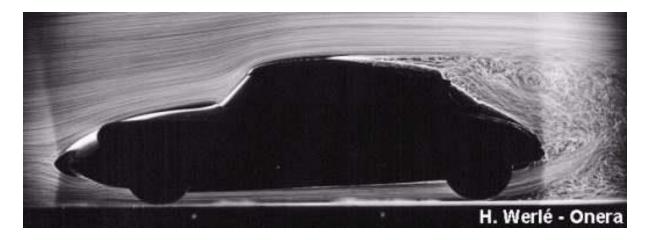
- The vehicle resistance forces include 3 types of forces
 - Aerodynamic forces (drag force)
 - Rolling resistance due to energy dissipation in tires, suspensions, shock absorbers, etc.
 - Grading resistance due to the slope of the road

Aerodynamic forces and moments

- The air flow around the vehicle during its motion creates aerodynamic forces that can become important especially at high speed
- The vehicle is a so-called bluff body which generates a lot of vortices and turbulent flows, especially at the level of back of the roof.
- The air flow is very complex because of
 - The ground effect that affects deeply the flow
 - The wheel spinning that interact strongly with the vehicle air flow.
 - The internal aerodynamic flow is necessary to cool the engine compartment and the air conditioning of the cabin, but it introduces a drag penalty

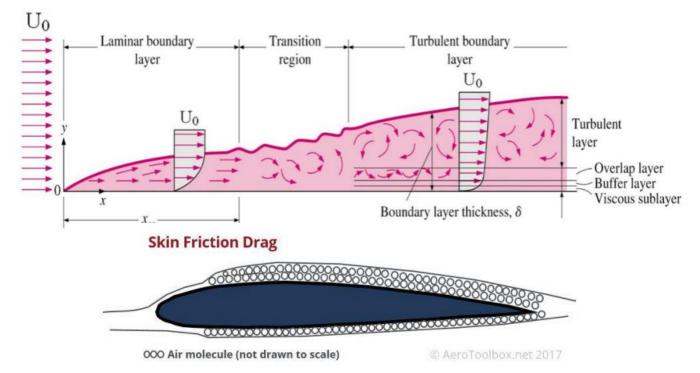
Aerodynamic forces and moments

- The aerodynamic forces have two major components:
 - <u>Shape drag</u>: the shape of the vehicle modifies the air flow creating a pressure distributions giving rise to a net force pointing backward Because of Mach and Reynolds numbers, the fluid flow is incompressible and non viscous (except in the boundary layers) Large vortices are present because of the bluff body geometry and the boundary layers are not attached



Aerodynamic forces and moments

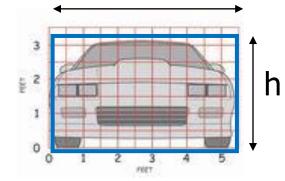
- The aerodynamic forces have two major components:
 - <u>Skin friction</u>: the viscosity effects, which take place in the boundary layers around the vehicle skin



Estimating the aerodynamic drag

Drag force

$$F_{AERO} = \frac{1}{2}\rho V^2 S C_x$$



t

- Estimating the frontal area
 - Using CAD system
 - Using pixel counting
 - Approximation: Paul Frere formula

$$S \simeq \psi h t \qquad \qquad \psi \simeq 0.83$$

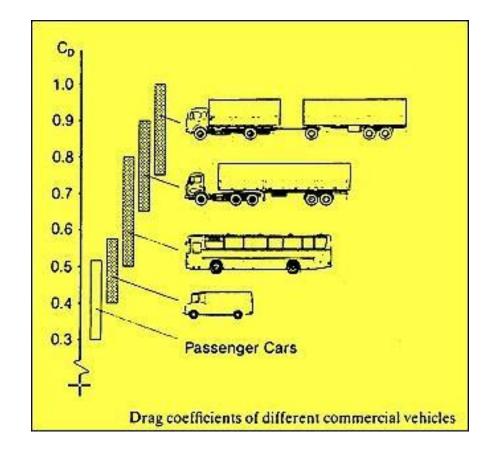
Typical drag coefficient of automobiles

TABLE 3.3 Values of Aerodynamic Resistance Coefficient for Various Types of Vehicle

Vehicle Type	Aerodynamic Resistance Coefficient C _D 0.3-0.52	
Passenger cars		
Vans	0.4-0.58	
Buses	0.5-0.8	
Tractor-semitrailers	0.64-1.1	
Truck-trailers	0.74-1.0	

Source: Reference 3.12,

(Wong Table 3.1)



Main sources of the drag of passenger car

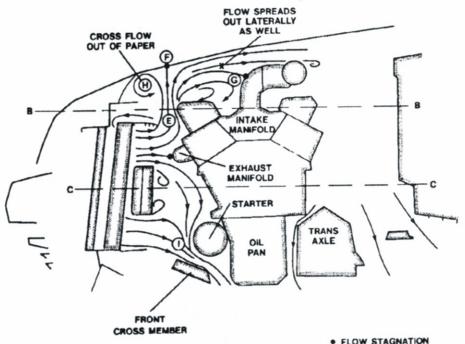
DRAG COEFFICIENT	TYPICAL		
COMPONENT	VALUE		
Forebody	0.05		
Afterbody	0.14		
Underbody	0.06		
Skin Friction	0.025		
Total Body Drag	0.275 65%		
Wheels and wheel wells	0.09		
Drip rails	0.01		
Window recesses	0.01		
External mirrors	0.01		
Total Protuberance Drag	0.12 28%		
Cooling system	0.025		
Total Internal Drag	0.025 6%		
Overall Total Drag	0.421		
VEHICLE OF THE 1980s			
Cars	0.30 - 0.35		
Vans	0.33 - 0.35		
Pickup trucks	0.42 - 0.46		

- 65% of drag comes from the body shape (front, back, floor, skin)
 - Large potential of reduction, especially for the back of the car to control the separation flows
- Influence as well of
 - Wheels (21%)
 - Details (7%)
 - Internal aerodynamics (6%)

¹ Based on cars of 1970s vintage.

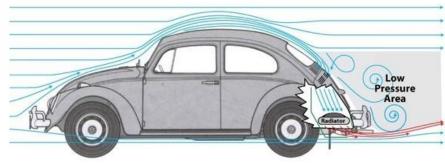
Gillespie Fig 4.11

Influence of air in engine compartment



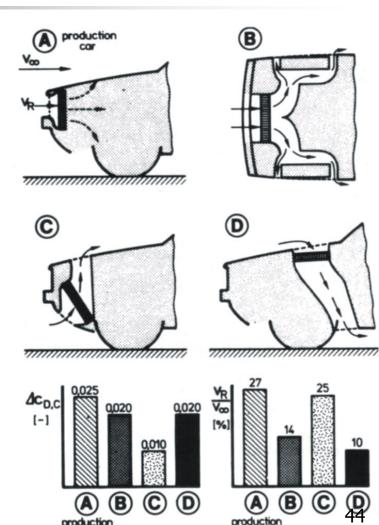
Gillespie: Fig 4.16 influence of engine cooling air flow

- The design of the air flow in the engine compartment has a major impact on the drag
- The air that is introduced loses its momentum giving rise to a net force
- The flow is very complex



Influence of air in engine compartment

- Design of engine cooling to allow the air to flow through the engine compartment with the minimum drag
- Reduction of air intakes to satisfy the needs



Gillespie: Fig 4.17 influence of engine cooling air flow

- Under free rolling conditions, it is necessary to apply a torque to maintain the motion and counteract the rolling resistance moment.
- The rolling resistance is covering a large number of phenomena of different natures:
 - The energy dissipation in the tire due to the hysteresis of the material due to alternate motion in the sidewalls and in the tread blocks
 - Air drag inside and outside the tire
 - The scrubbing of the tire on the ground
 - The friction in the driveline
 - The dissipation of energy in the shock absorber
 - The misalignment of the tires, the longitudinal and lateral slip
 - The deformation of the road surface

 Experiments show that generally, the global rolling resistance force are with a very good agreement using a linear model as a function of the vertical force applied onto the tire

$$F_{RR} = f_{RR} F_z = f_{RR} mg \cos \theta$$

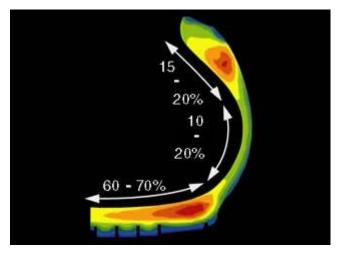
The coefficient f_{RR} is the rolling resistance coefficient

The rolling resistance coefficient, ratio between the rolling resistance force and the normal force encompasses the complicated and interdependent physical properties of the tire and the ground.

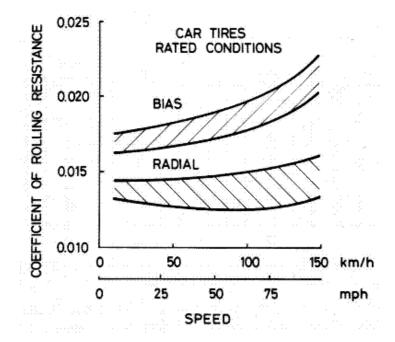
 <u>1st cause</u>: hysteresis of the tire materials (viscoelastic rubber) because of deformation cycle

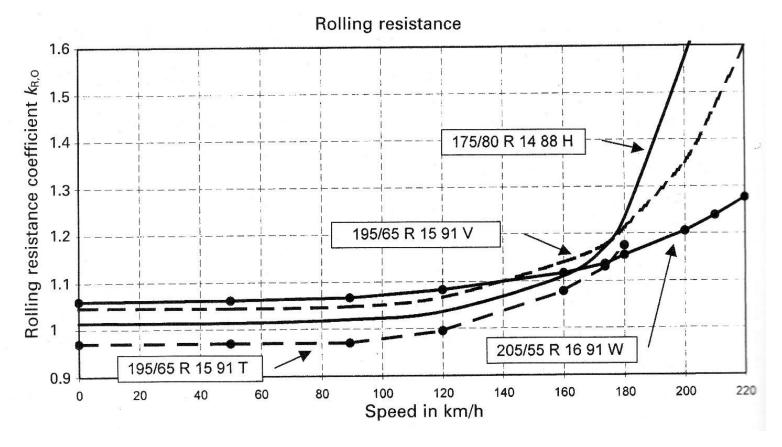
Other sources:

- Frictions during slippage
- Air ventilation inside and outside
- Example: truck tire at 130 km/h
 - 90-95 % = hysteresis
 - 2-10 % friction
 - 1.5 3.5 % aerodynamic dissipation



- The rolling resistance is influenced by the tire structure:
 - The rolling resistance of bias tire is higher than radial tire

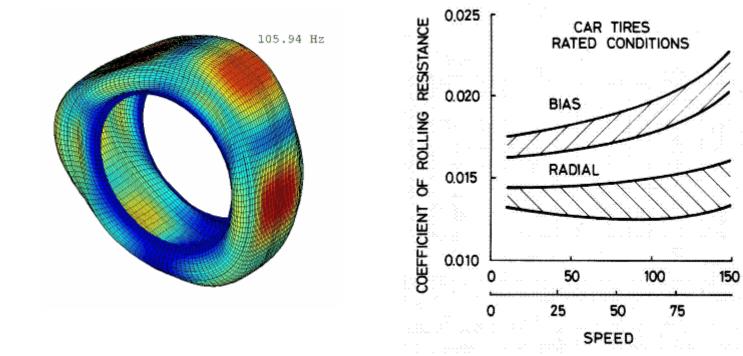




Influence of load index

The operating conditions mainly:

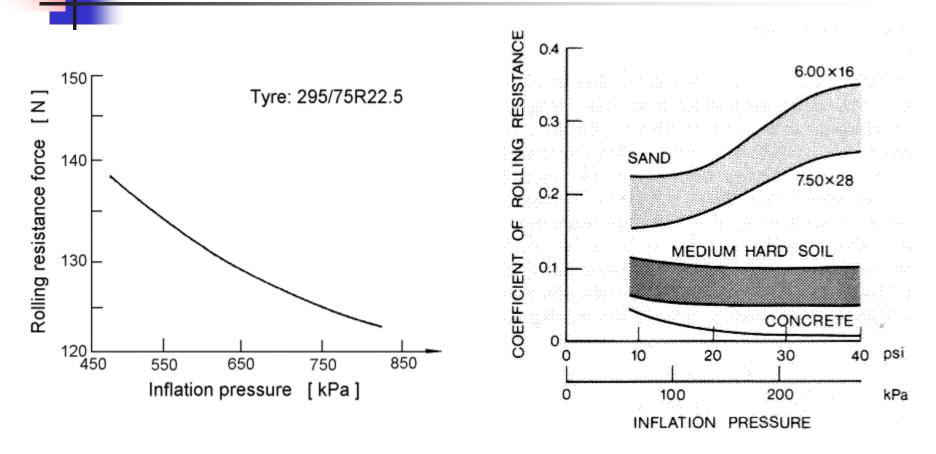
- The <u>inflating pressure</u>: the rolling resistance is reduced for a higher inflation pressure
- The <u>vehicle speed</u>: one observes a slight increase with v at low speed. A dramatic increase after a critical speed because of the development of high-energy standing waves
- <u>The longitudinal and lateral slip</u>: the rolling resistance increases as the square of the side slip.
- <u>The rolling resistance is much higher on soft and smooth</u> ground because of the deformation work of the soil
- The rolling resistance is also higher on wet ground or in snow



Influence of speed

km/h

mph



Influence of inflation pressure

Influence of the terrain stiffness

Estimation of rolling resistance coefficient

 A typical formula given by Wong Radial tires for passenger cars with a nominal inflation pressure p and smooth road profile:

 $f_{RR} = 0,0136 + 0,4 \ 10^{-7} \ V^2$ V in km/h

Approximation provided by tables (ex Automotive handbook, Bosch)

Road surface	Coefficient of rolling resistance f	
Pneumatic car tires on Large sett pavement		0.015
Small sett pavement Concrete, asphalt		0.015 0.013
Rolled gravel	14	0.02
Tarmacadam	1.12.81	0.025
Unpaved road Field	0.05	
Pneumatic truck tires on		
concrete, asphalt	0.0060.01	
Strake wheels in field	0.140.24	
Track-type tractor	1	
in field	0.070.12	
Wheel on rail	0.0010.002	

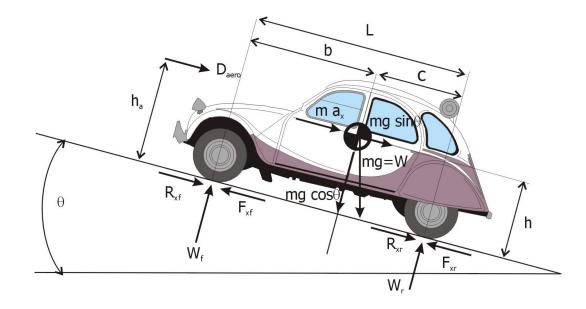
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$$f_{RR} = f_0 + f_2 V^2$$

Resistance force due to grading

• Expression of grading resistance

$$F_{grading} = mg \sin \theta$$



Expression of road load

General form of the vehicle resistance

 $F_{RES} = F_{AERO} + F_{RR} + F_{GRADE}$

General formulation

$$F_{res} = A + Bv^2$$

• with A, B > 0 $A = m g \cos \theta f_0 + m g \sin \theta$ $B = 1/2 \rho S C_x + m g \cos \theta f_2$

Evolution of road loads with vehicle speed

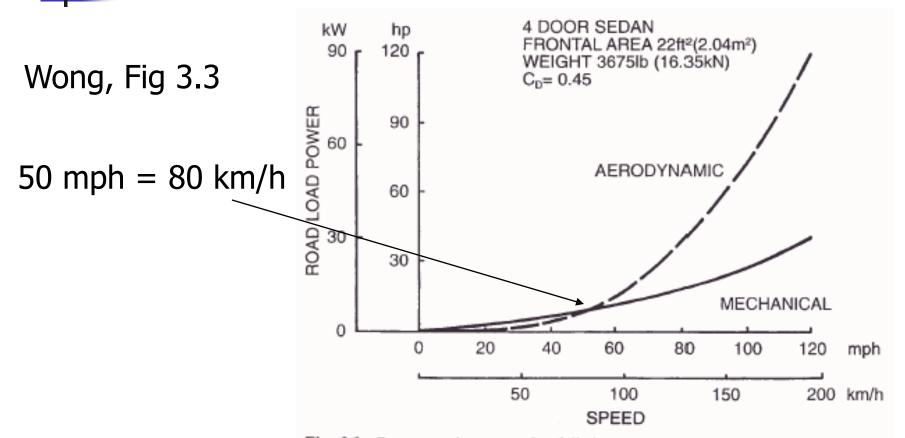


Fig. 3.3 Power requirements of a full-size passenger car as a function of speed. (Reproduced with permission of the Society of Automotive Engineers from reference 3.1.) 56